

Recent advances in pulsed-mode measurements at CERN

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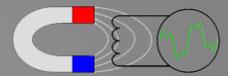
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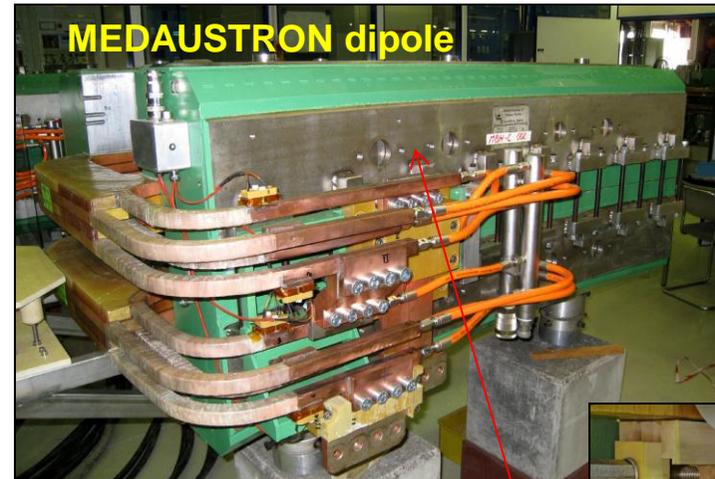
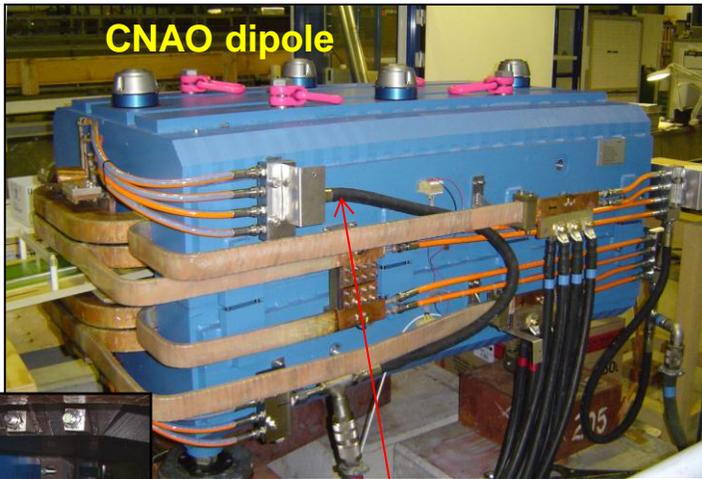
Overview

Pulsed-mode measurement with fixed coil:

- 1) Eddy current studies of dipoles for a hadrontherapy synchrotron (MedAustron)
- 2) High frequency field fluctuations in the Proton Synchrotron's main magnets
- 3) Experimental determination of inductance in resistive magnet



Eddy current studies of dipoles for a hadrontherapy synchrotron (MedAustron)



**Main magnets designs differences
influencing Eddy currents**

CNAO

Iron made (magnetic) tension bars

7 small blocks for shimming adjustment

No Rogowski profile for shims

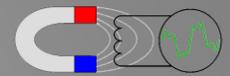


MedAustron

Stainless steel (non magnetic) tension bars

5 large blocks for shimming adjustment

Rogowski profile for shims



Design options and benefits:

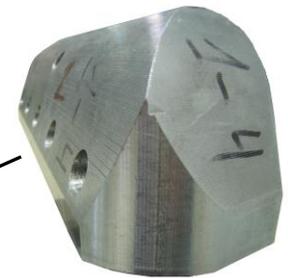
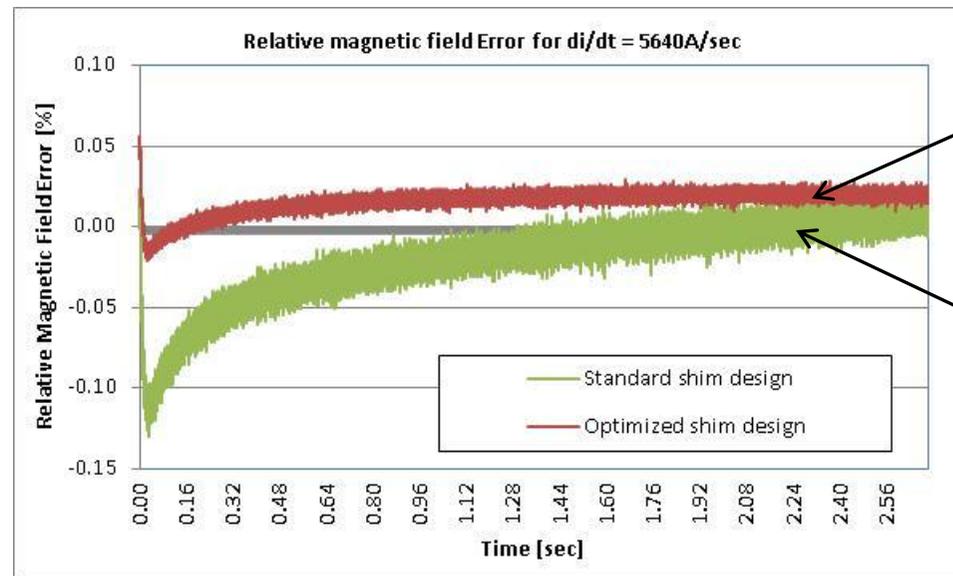
Stainless steel tension bars justification

- A previous study on CNAO magnets did show a strong influence on Eddy current at magnet saturation
- Eddy currents created in tension bars have a long decay time

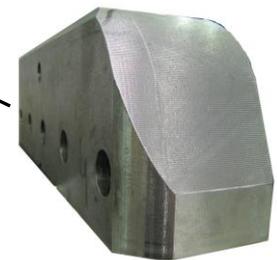
Shims with Rogowski profile interest

- They limit the end field component on the Z axis, which create Eddy currents in shims
- Eddy currents created in shims have a short decay time

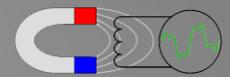
Eddy currents effects amplitude variation of $+ 1.10^{-3}$ between the two types of shims



Optimized shim



Standard shim



Results comparison between the two types of dipoles for Eddy currents effects on the integrated field:

- **Amplitude** of Eddy currents effects :

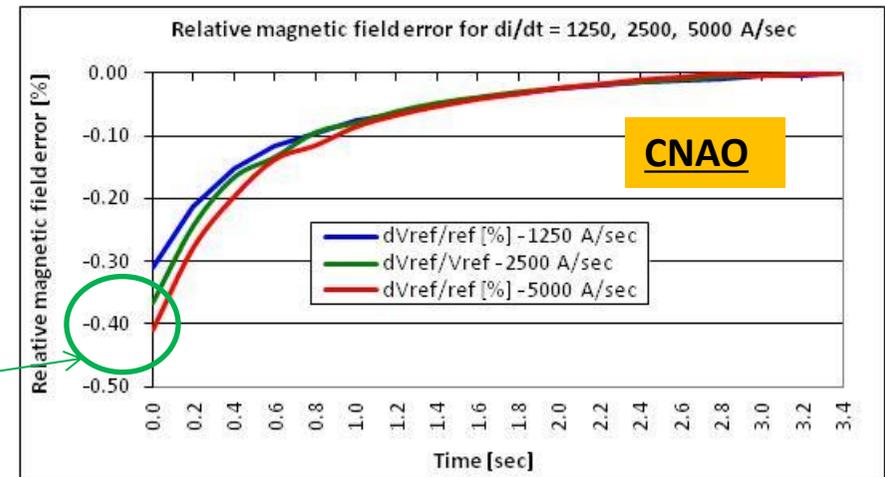
→ 16 times lower on MedAustron dipoles

CNAO = 0.4 %

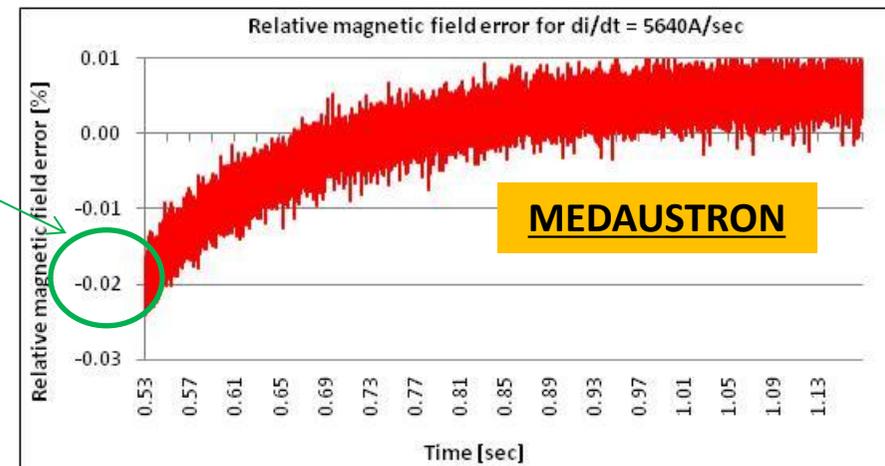
MedAustron = $2,5 \cdot 10^{-4}$

- **Time constant** of Eddy currents effects :

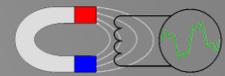
→ ≈ 4 times lower on MedAustron dipoles



CNAO $\tau = 0.65$ sec

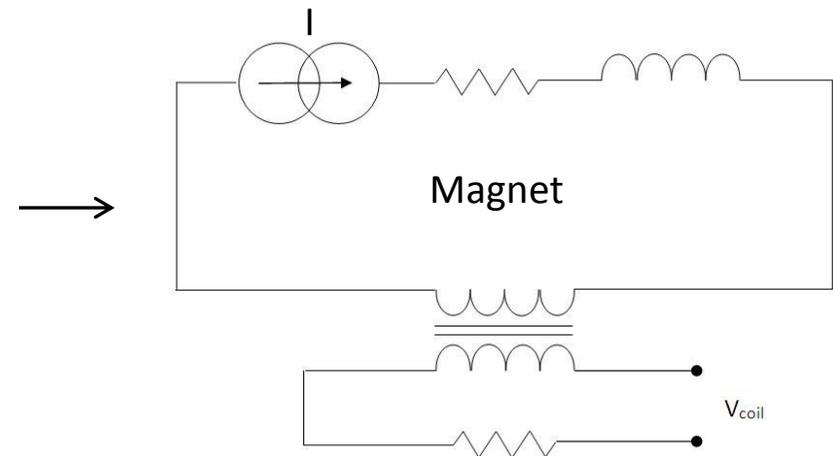


MedAustron $\tau = 0.15$ sec

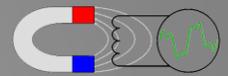


High frequency field fluctuations in the Proton Synchrotron's main magnets 1/3

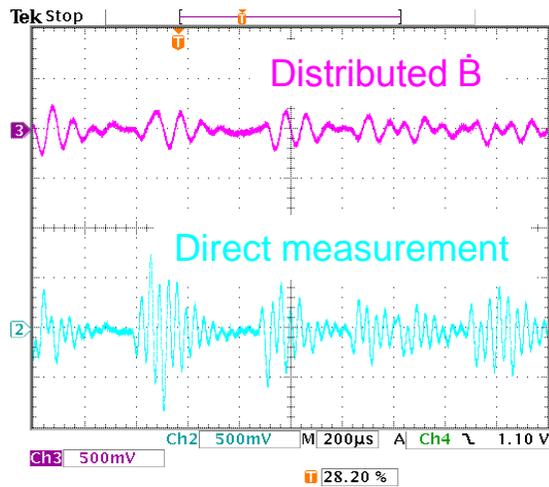
- PS operation team reported high level of noise on the \dot{B} signal of the real-time field measurement system (B-train) → stability of RF feedback, beam position
- Measurement campaign done inside magnet gap with a fixed coil. Where does the observed noise come from ?



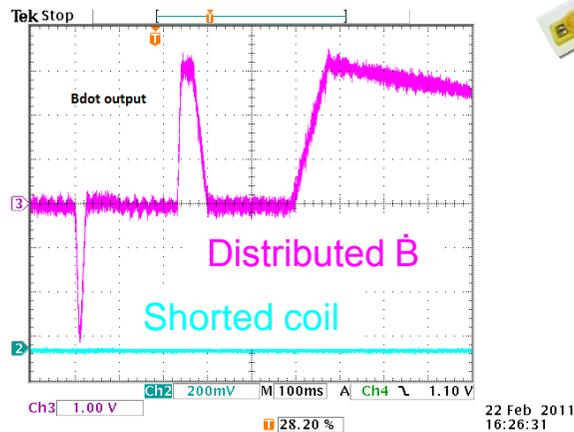
Electrical circuit: AC source, R, L inductive coupling to coil



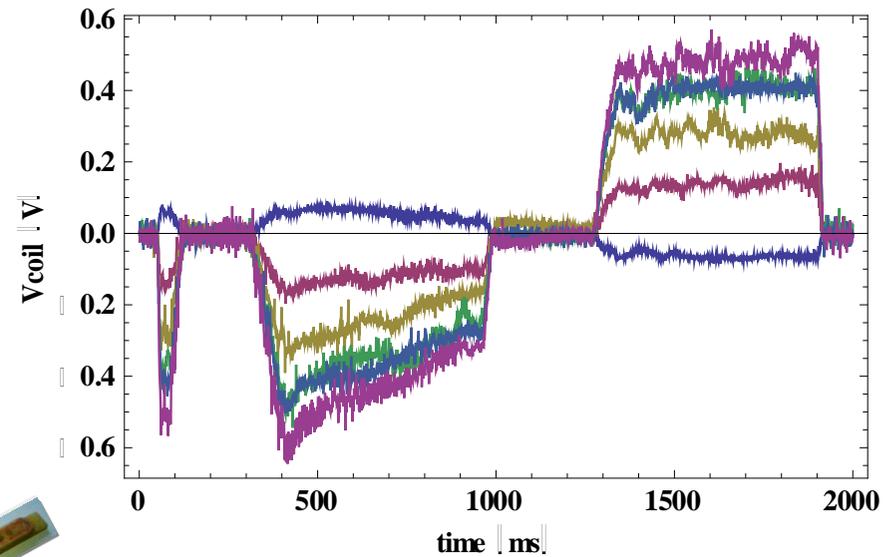
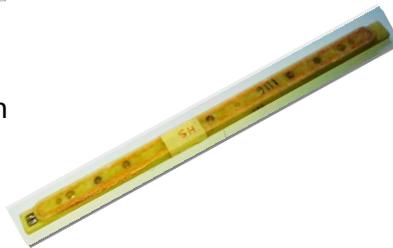
High frequency field fluctuations in the Proton Synchrotron's main magnets 2/3



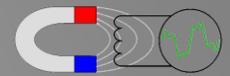
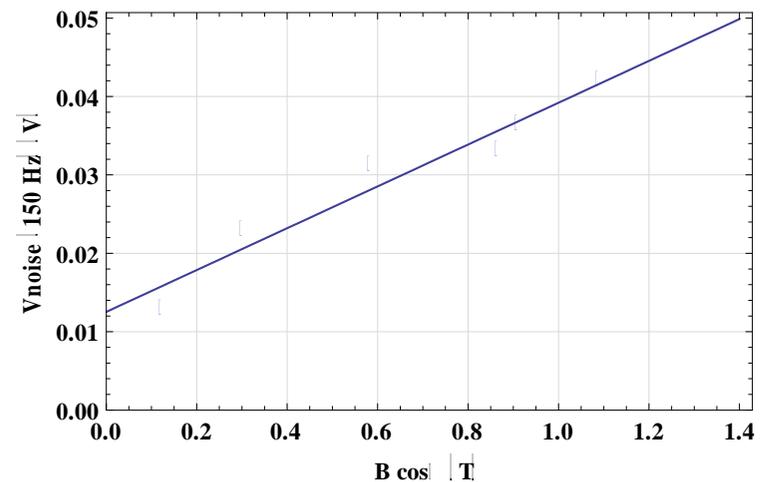
Measurement consistent with local
8 kHz LPF → noise not due to distribution



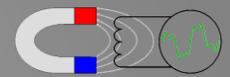
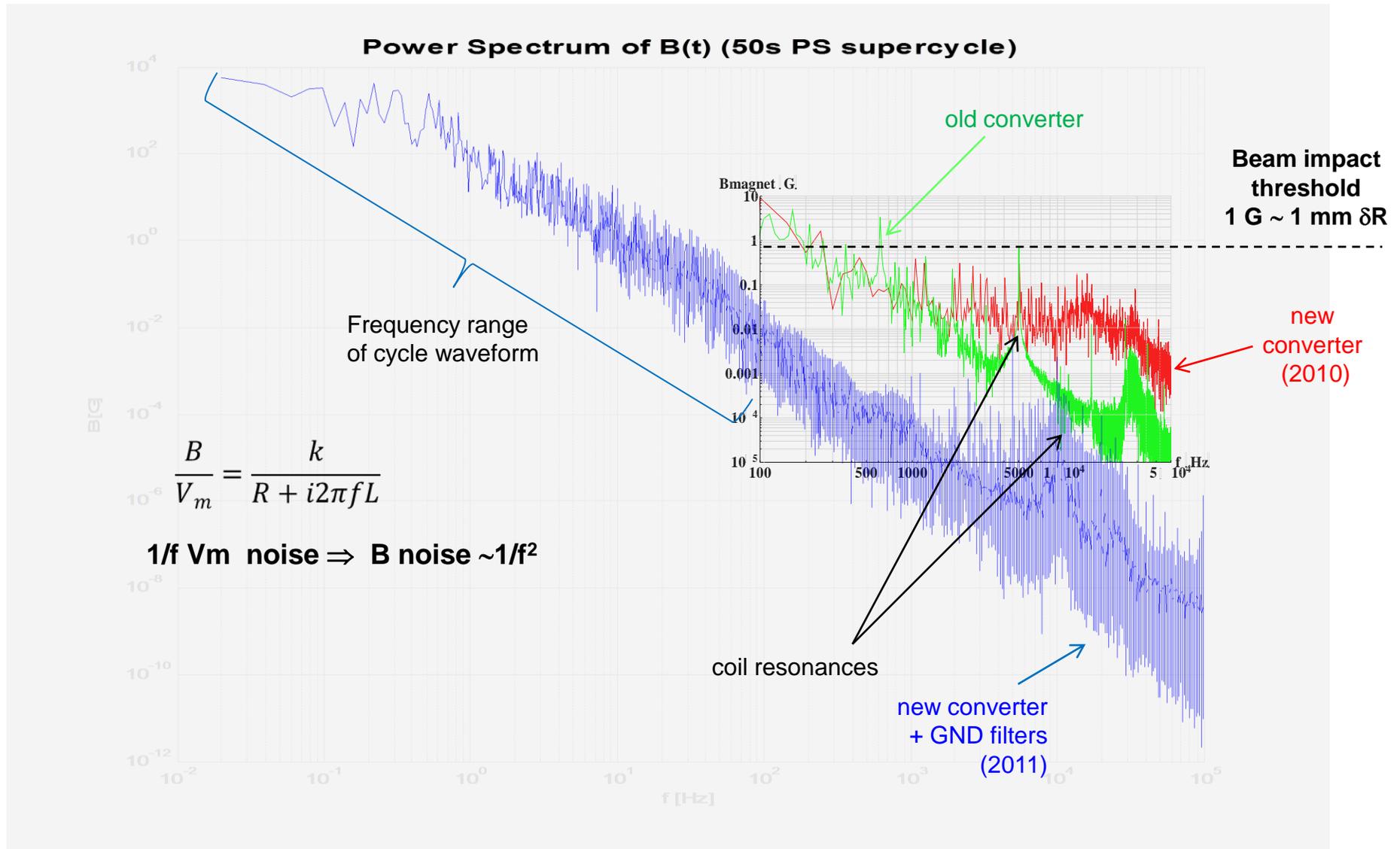
Noise drops in shorted coil
→ not due to acquisition system



As the coil is turned from perpendicular to parallel to field,
the noise varies linearly with the signal level
→ the **noise mostly reflects actual magnetic field fluctuations**



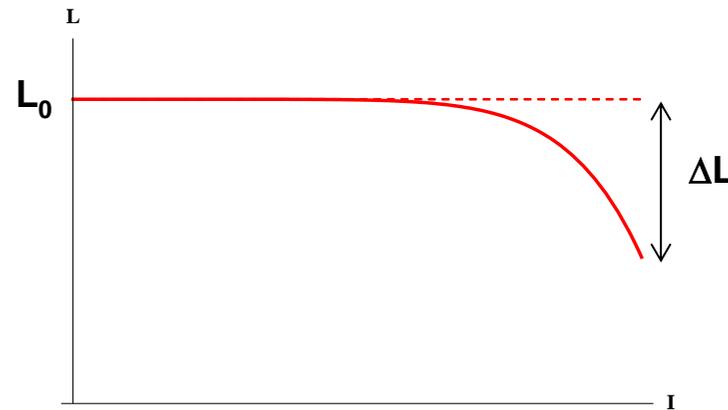
Converter evolution and effects on the noise



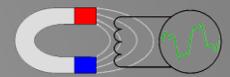
Magnet inductance knowledge → essential for fast-cycled magnets

- Accurate knowledge of the load → **improve** the stability of the **current control** during operation
- Accelerator magnets behave electrically like **very large inductors**
- **Resistive magnet** → iron core **saturation** → **inductance non-linearity**

General qualitative behavior of magnet inductance L vs. excitation current I



- Main aim of this experimental determination: establish L drop due to saturation at high current
- Several definitions of inductance → all coincide in linear case , **all diverge at high field** (saturation)



Experimental determination of inductance in resistive magnet 2/6

Simplified electromagnetic model:

- Typical resistive magnet → excitation coil producing magnetic flux + iron yoke with relative permeability that channels the flux to an air gap.

Some of the flux leak out of the iron depending of field level and geometry

Inductance :

L = Apparent inductance

Ratio between excitation current and total flux crossing the coil.

L_d = Differential inductance (or incremental inductance)

Incremental ratio of flux to current or as the ratio of the inductive voltage to the current ramp rate .

L_w = Energy equivalent inductance

Inductance related to the energy stored in the magnetic field. It can be evaluated from measurements of V and I .

L_g = Gap inductance

Inductance due to the energy in the air gap.

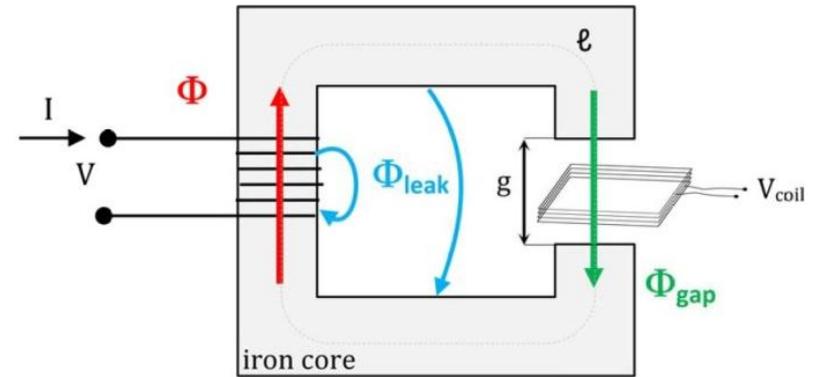


Fig. 2 - Schematic representation of a resistive dipole magnet

$$\text{Field in the gap : } B = \frac{\mu_0 \mu_r N I}{l + \mu_r g}$$

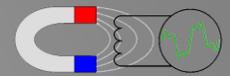
$$L = \frac{\Phi}{I}$$

$$L_d = \frac{d\Phi}{dI} = \frac{V - RI}{\frac{dI}{dt}}$$

$$L_w = \frac{2}{I^2} \int_0^t (V - RI) I dt$$

$$L_g = \frac{1}{\mu_0} \left(\frac{B}{I} \right)^2 g a l_m$$

g = air gap
 a = air gap width
 l_m = magnetic length
 μ_0 = vacuum perméabilité



Experimental determination of inductance in resistive magnet 3/6

Simulated L , L_d and L_w :

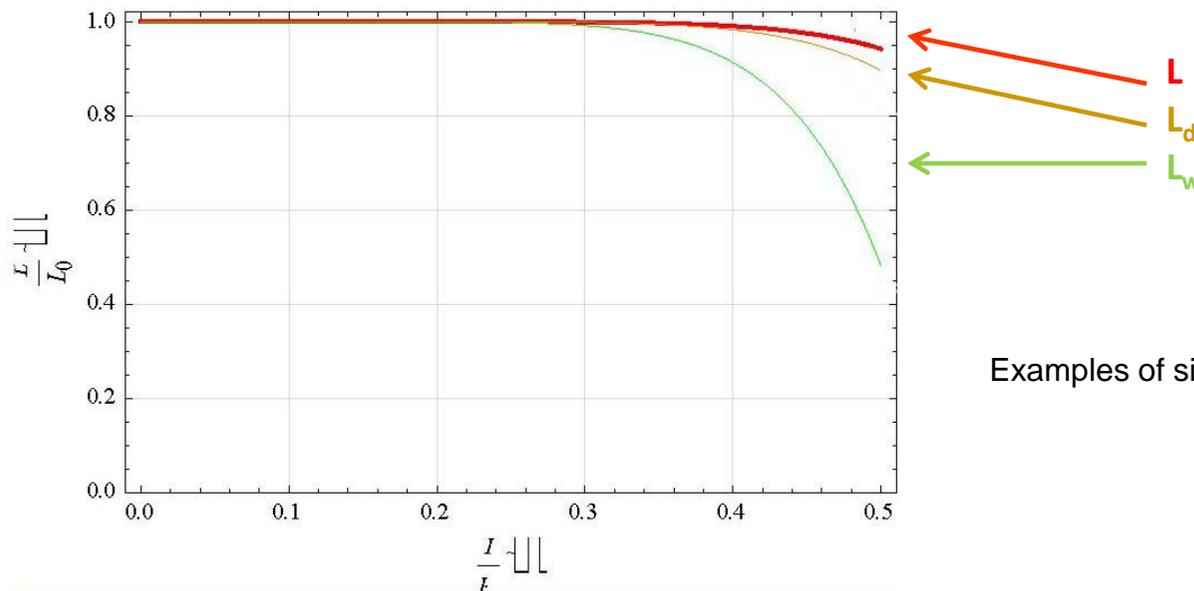
The link between the different definitions of inductance can be clarified by taking this simple expression for $L(I)$ in closed form.

$$L(I) = L_0 \left(1 - \left(\frac{I}{I^*} \right)^n \right) \rightarrow \text{if } n \text{ sufficiently high (which describe magnets with delayed, but sharper saturation)}$$

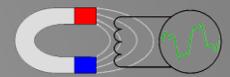
this expression fit experimental data reasonably well

By substitution of $L(I)$ in the previous expression of L_d and L_w we can simulate the curves below and deduce that:

- Effects of saturation in $L_d(I)$ and $L_w(I)$ **are always proportional to the effect in $L(I)$** , irrespective of the current.
- Drop of **energy equivalent** inductance L_w tends to a **limit magnitude** $\Delta L_w \rightarrow 2\Delta L$
- Drop of the **differential inductance** grows **unbounded**

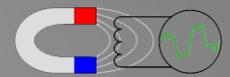


Examples of simulated $L(I)$, $L_d(I)$ and $L_w(I)$ curves for $n=10$



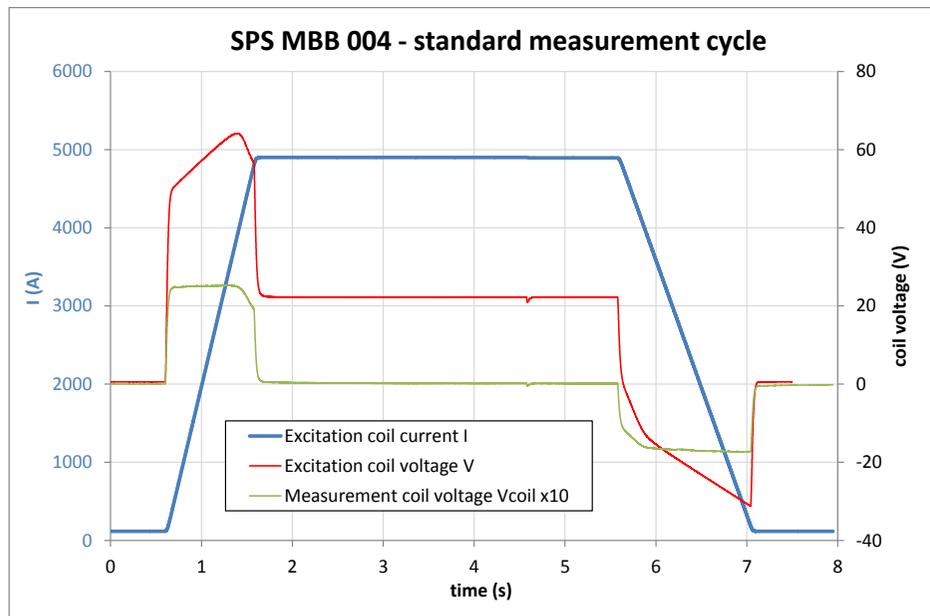
Measurement procedure (on main SPS dipole type MBB):

- All the above defined versions of the inductance **can be derived from a continuous measurement of excitation current $I(t)$ and voltage $V(t)$** . (Acquired with an ADC NI 16 bits USB 6216, 20 kHz sampling)
- Current was read on power supply DCCT, and voltage drop through connectors fixed onto the main current leads, in order to improve the accuracy of the resistance measurement.
- $V_{coil}(t)$ induced on an integral pick-up coil inserted into the magnet was measured in order to estimate the magnetic field energy in the gap.
- Test done on standard measurement current cycle. (Saturation can be seen close to 4000 A).
- Coil resistance checked by taking the average of the V/I ratio on the flat-top (where both inductive voltages and eddy currents effects are negligible).
- Measurement done after cycling continuously the magnet in order to simulate the thermal conditions of the machine in operation.

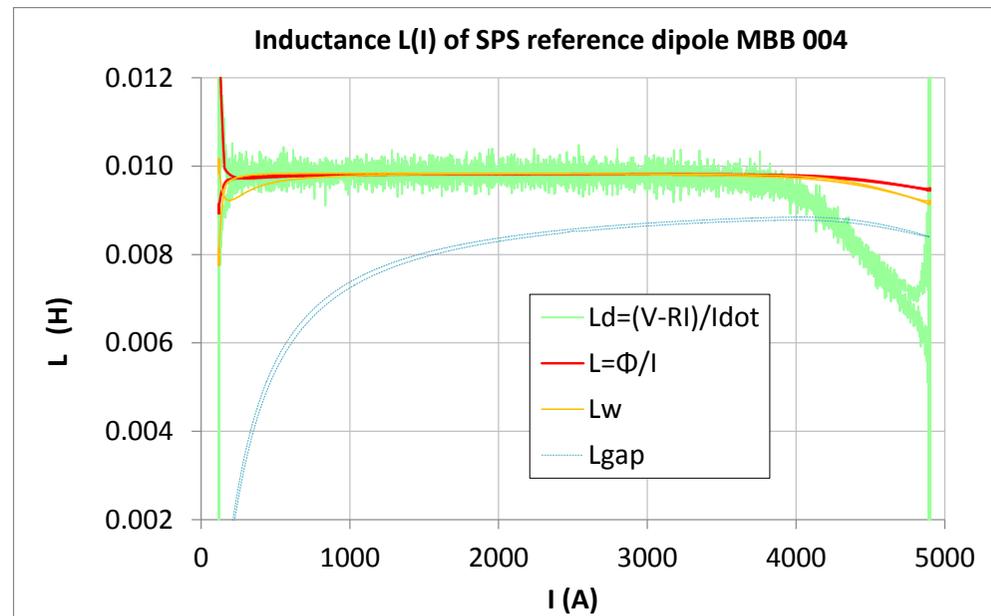


Experimental determination of inductance in resistive magnet 5/6

Plotted results of the four versions of the inductance computed after measurements :



Signals measured at 20 kHz during a SPS reference MBB current cycle.
(Green curve (Vcoil) magnified by a factor 10)



Comparative plot of the apparent, differential, energy equivalent and gap inductances

The drop of the differential (L_d) and energy equivalent (L_w) inductance is respectively:

$$\frac{\Delta L_d}{L_0} \approx 39.4\%$$

$$\frac{\Delta L_w}{L_0} \approx 7.2\%$$

Conclusion:

- For MBB dipole a **magnetic field saturation** of just **3.4%** corresponds to a differential **inductance saturation** of almost **40%**.
 - A large drop of the differential inductance at saturation is to be expected **even for magnets which limited saturation**.
 - **Divergence** between differential and apparent inductance **grows larger for magnets which exhibit sharper saturation** at higher current
 - In case such measurement is not possible **the drop of differential inductance may be predicted from the magnetic field behavior**, at the price of additional uncertainty due to the leaking flux fractions λ_{coil} and λ_{yoke}
 - Measurement of the inductance curves can be done when necessary on the test bench in parallel with standard magnetic tests, adding little cost to the test program.
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